

Intelligent Omni Surface-Assisted Self-Interference Cancellation for Full-Duplex MISO System

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Abstract—The full-duplex (FD) communication can achieve higher spectrum efficiency than conventional half-duplex (HD) communication; however, self-interference (SI) is the key hurdle. This paper is the first work to propose the intelligent omni surface (IOS)-assisted FD multi-input single-output (MISO) FD communication systems to mitigate SI, which solves the frequency-selectivity issue. In particular, two types of IOS are proposed, energy splitting (ES)-IOS and mode switching (MS)-IOS. We aim to maximize data rate and minimize SI power by optimizing the beamforming vectors, amplitudes and phase shifts for the ES-IOS and the mode selection and phase shifts for the MS-IOS. However, the formulated problems are non-convex and challenging to tackle directly. Thus, we design alternative optimization algorithms to solve the problems iteratively. Specifically, the quadratic constraint quadratic programming (QCQP) is employed for the beamforming optimizations, amplitudes and phase shifts optimizations for the ES-IOS and phase shifts optimizations for the MS-IOS. Nevertheless, the binary variables of the MS-IOS render the mode selection optimization intractable, and then we resort to semidefinite relaxation (SDR) and Gaussian randomization procedures to solve it. Simulation results validate the proposed algorithms' efficacy and show the effectiveness of both the IOSs in mitigating SI compared to the case without an IOS.

Index Terms—Full-duplex communication, self-interference cancellation, intelligent omni surface, MISO communication, semidefinite relaxation, non-convex optimization.

I. INTRODUCTION

The full-duplex (FD) communication has been developed to meet the ever-increasing traffic demand for wireless communications. Unlike the conventional half-duplex (HD) communication, FD communication can ideally double the ergodic capacity since it can transmit and receive in the same time slots and frequency band [1, 2]. It not only improves the ergodic capacity, but also enhances network secrecy [3] and reduces signalling overhead, and end-to-end delay [4]. Thanks to these features, FD communication has gained much attention from industry and academia. In [5], the authors applied multiple FD nodes to maximize the sum-rate of the nodes by jointly optimizing the subcarrier assignment and power allocation. Also, a

novel two-phase protocol was proposed in a wireless communication FD network which ensured uninterrupted information transmissions and self-energy recycling by exploiting the features of FD nodes [6]. An FD receiver was introduced in the mmWave communication network [7] to cover the presence of a transmitter in the presence of a watchful warden by jointly optimizing the beamforming, transmit power and jamming. Besides, the authors of [8] investigated an FD relay in device-to-device communications underlying a cellular network from both analysis and optimization perspectives. To boost the sum-throughput and reduce the total energy of Internet-of-Things networks, a rotary-wing unmanned aerial vehicle equipped with an FD access point was introduced [9]. In addition, the authors of [10] utilized a double deep Q-network to solve the throughput maximization and secrecy rate maximization problems in a secure cognitive radio relay network where the relay nodes operated in the FD mode and transmitted jamming signals to the eavesdropper. Furthermore, an optimal power allocation strategy was proposed for the dual-hop FD decode-and-forward relay system to minimize the outage probability. However, the FD system cannot achieve the ideal performance due to the self-interference (SI) [11].

As a downside of FD communications, SI imposed by the devices' own transmissions cannot be neglected. The SI, if left unattended, could result in reduced capacity for FD systems that fall below that of HD systems [2]. Fortunately, self-interference cancellation (SIC) techniques have been exploited to tackle this issue. The SIC techniques can be classified into three steps: passive suppression, analogue cancellation and digital cancellation. The passive suppression relies on a large physical distance between transmit and receive antennas, thus high isolation can be achieved [12]. Secondly, the analogue cancellation exploits the degrees of freedom bestowed by antenna arrays. Specifically, the beam patterns of transmitters can be designed to suppress the signal strength received at the receive antennas [13, 14]. Furthermore, the digital cancellation technique applies digital cancellation protocols, such as ZigZag [15] to mitigate residual SI further. The authors of [16] proposed a novel digital SIC technique to mitigate the SI signal and the transmitter and receiver impairments. However, conventional RF cancellation techniques are frequency-selective due to analogue SI cancellation circuits, such as Balun, i.e., the best cancellation result can be achieved at the centre frequency, and the SIC result is not promising for frequency components that are far apart from the centre frequency [17]. This imposes severe bandwidth limitations for FD radio, which would fail to operate at high-frequency bands such as millimetre waves.

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Other problems include implementation complexity and large insertion loss associated with RF SIC circuits. In addition, it was demonstrated that the operational bandwidth and the performance of RF-based cancellation were usually restricted by the hardware [18]. Moreover, although SI can be reduced via designing the beam pattern of the transmitter [19], the size, weight, and power (SWaP) limitations of small devices do not allow the deployment of enough RF units to achieve flexible and efficient FD transmissions [20]. In a nutshell, the SIC is still a key hurdle to FD communications to double the channel capacity for wireless communication networks.

In recent years, the reconfigurable intelligent surface (RIS) has been exploited to meet the increasing demands for future sixth-generation (6G) wireless networks because it can enhance the performance of wireless communication at low costs. In principle, RIS is constructed by a number of components whose electromagnetic responses can be adjusted to enhance a given performance metric [21]. The research regarding RIS has been spreading in various areas such as unmanned aerial vehicle communications [22], cooperative networks [23], dual-function radar communication systems [24], physical layer security enhancement [25]. In particular, RIS supports wide frequency bands such as mmWave, the authors of [26] demonstrated that the RIS was capable of improving the sum-rate of the proposed mmWave systems. More recently, the authors of [27] conceived a multiple-access framework for RIS-assisted communications which improves MAC efficiency, reduces the computational complexity of RIS as well as offers fairness for multiple users. In addition, by training and deploying a multi-task learning model at a RIS controller, [28] efficiently maximized the throughput of RIS-assisted aerial-terrestrial communications.

Moreover, it has been demonstrated that the utility of RISs in FD communications can enhance the performance of wireless communication networks [29, 30]. For example, the weighted sum rate of the multi-input multi-output (MIMO) communication system with an FD base station can be improved by introducing a RIS [31]. Additionally, the weighted sum transmit power consumption of the base station and uplink user can be greatly reduced by jointly optimizing their transmit power, and the phase shifts [32], subject to the rate constraints at the users and uni-modulus constraints at the RISs. Furthermore, the authors studied the RIS technology in an FD wireless communication system where the outage and error probabilities were derived [33]. More specifically, the authors provided some insights into how to enhance the performance and save energy consumption, via obtaining the closed-form expressions of ergodic capacity and symbol error rate, in the RIS-assisted FD systems [34]. Besides, the authors of [35] investigated a RIS-aided FD wireless communication system and demonstrated that the RIS was capable of enhancing the performance of FD systems with a large number of elements when the SI cannot be ideally removed. Notice that the above works only use the RISs to enhance signal strength at the receiver, and they have not utilized the RIS to balance the SIC and data transmission. In addition, all of the above works assumed that the traditional SIC techniques could eliminate the SI instead of mitigating the SI with the assistance of RISs.

Therefore, the aforementioned frequency-selectivity and SWaP problems for the conventional SIC schemes have not yet been well addressed.

To tackle this problem, we utilize the intelligent omni surface (IOS), which was developed by NTT DOCOMO INC. to achieve reflection and refraction in 360-degree coverage [36], in reducing SI as well as boosting the transmission rate of FD communication networks, and solving the bandwidth constraint and SWaP limitation incurred by traditional SIC techniques. Also, the authors of [37] investigated the performance of an IOS in a downlink communication system, however, the full-duplex transmissions and the impact of IOSs on the self-interference cancellation were not considered. To the best of our knowledge, this work is the first of its kind to establish an IOS-aided FD multi-input single-output (MISO) wireless communication network in canceling SI and enhancing data rate. Specifically, we consider two modes of the IOS, namely, energy splitting (ES)-IOS and mode selection (MS)-IOS, to maximize the downlink data rate while minimizing the SI power, subject to the downlink rate thresholds. The main contributions of this paper are summarized as follows:

- 1) We propose a novel IOS-aided MISO FD communication network and introduce two types of IOS, ES-IOS and MS-IOS. The proposed schemes not only can enhance the data rate at the destination but also mitigate the SI and against the frequency-selectivity and SWaP limitations issues that exist widely in the traditional SIC schemes.
- 2) We investigate two optimization problems, including downlink rate maximization and SI power minimization problems. Firstly, we aim to maximize the downlink rate at the destination, subject to the transmit power, uplink rate threshold, and phase shift constraints. On the other hand, SI power is minimized, subject to the downlink rate threshold, transmit power and phase shift constraints.
- 3) We utilize alternative algorithms for two non-convex problems with different types of IOS to solve the sub-problems iteratively. The quadratically constrained quadratic programming (QCQP) method is applied to solve the beamforming, joint amplitudes and phase shifts optimizations with the ES-IOS as well as the phase shifts optimizations with the MS-IOS. Besides, we resort to the semi-definite relaxation (SDR) and Gaussian randomization methods to solve the binary optimizations for the cases with MS-IOS.
- 4) Simulation results validate the efficiency of the proposed algorithms and demonstrate the flexibility and effectiveness of the utility of IOS to strike a good balance between SIC and data transmission for FD MISO communication networks. More specifically, we show that the SI can be reduced to a limited region by IOSs. At the same time, the data rate requirement is guaranteed for ES-IOS and MS-IOS, which shows the effective implementation of IOS in MISO FD communication networks.

The remainder of this paper is organized as follows. Section

II presents the system model of our proposed IOS-assisted MISO FD communication system and the problem formulations. Section III maximizes the data rate at the destination by optimizing the beamforming vectors of the transmitter, the amplitudes and phase shifts of the ES-IOS, and the mode selection and phase shifts of the MS-IOS, iteratively. Section IV presents the SI power minimization for the cases with ES-IOS and MS-IOS, respectively. Section V presents numerical results to validate the efficiency of our proposed algorithms and the merits of applying IOS to the MISO FD communication system. Finally, Section VI concludes this paper.

Notations: In this paper, scalars are denoted by italic letters, and vectors and matrices are denoted by bold lowercase letters and bold uppercase letters, respectively. \mathbf{a}^H gives the Hermitian of the vector \mathbf{a} , \mathbf{a}^T and \mathbf{a}^* denote its transpose and conjugate operators, respectively. $[\mathbf{A}]_{i,j}$ is the element located on the i th row and j th column of matrix \mathbf{A} , $[\mathbf{a}]_i$ is the i th element of vector \mathbf{a} . $\mathbf{B} \odot \mathbf{C}^T$ is the Hadamard product of \mathbf{B} and \mathbf{C} . The trace of a matrix \mathbf{A} is represented by $\text{Tr}(\mathbf{A})$. $\text{Re}\{\cdot\}$ denotes the real part of a complex value, $\mathbf{1}_M$ stands for the $M \times 1$ identity vector. $\text{diag}\{\cdot\}$ and $(\cdot)^*$ denote the operator for diagonalization and the optimal value, respectively and $\mathcal{O}(\cdot)$ is the big-O notation.

II. SYSTEM MODEL AND PROBLEM FORMULATION

A. System model

We design an IOS-assisted FD MISO communication network where the transmitter sends signals to the single-antenna destination with the assistance of a L -element IOS; and simultaneously design the phase shifts of the IOS to mitigate the SI between the receive antennas and the transmit antennas. The transmitter is equipped with M transmit antennas and N receive antennas and is integrated with an IOS. Furthermore, two types of IOSs are employed: 1) ES-IOS, the elements capable of reflecting and refracting signals simultaneously, as illustrated in Fig. 1(a). 2) MS-IOS¹, where each element can only reflect or refract signal at one-time slot, is illustrated in Fig. 1(b). In addition, the reflecting and refracting phase shifts coefficient matrices of the ES-IOS are represented as $\Theta_e = \text{diag}\{a_{e,1}e^{j\alpha_{e,1}}, a_{e,2}e^{j\alpha_{e,2}}, \dots, a_{e,L}e^{j\alpha_{e,L}}\} \in \mathbb{C}^{L \times L}$ and $\Phi_e = \text{diag}\{b_{e,1}e^{j\beta_{e,1}}, b_{e,2}e^{j\beta_{e,2}}, \dots, b_{e,L}e^{j\beta_{e,L}}\} \in \mathbb{C}^{L \times L}$, where $a_{e,l}$, $b_{e,l}$ denote the reflecting and refracting amplitudes at the l th element, $l = 1, 2, \dots, L$, and $\alpha_{e,l}$, $\beta_{e,l}$ indicate the phase shifts of the l th element, respectively. Hence, according to [37], the constraints² for the ES-IOS can be given by

$$a_{e,l}^2 + b_{e,l}^2 \leq 1, \quad (1a)$$

$$0 \leq a_{e,l}, b_{e,l} \leq 1, \quad (1b)$$

¹It is worth mentioning that the MS-IOS is more readily implementable than the ES-IOS because of the low hardware design complexity, while the ES-IOS provides higher flexibility [38]; in addition, the phase shifts for reflection and refraction can generally be chosen independently of each other for both cases. Therefore, in this paper, we investigate both cases.

²Note that continuous phase shifts are considered in this paper, similar to [30–32], which is the upper bound of the system performance. Besides, the discrete phase shifts can be derived by quantifying the obtained optimal continuous phase shifts, which will be shown in Section V.

$$0 \leq \alpha_{e,l}, \beta_{e,l} \leq 2\pi, \quad \forall l. \quad (1c)$$

On the other hand, the reflecting and refracting phase shifts coefficient matrices of the MS-IOS are denoted as $\Theta_m = \text{diag}\{a_{m,1}e^{j\alpha_{m,1}}, a_{m,2}e^{j\alpha_{m,2}}, \dots, a_{m,L}e^{j\alpha_{m,L}}\} \in \mathbb{C}^{L \times L}$ and $\Phi_m = \text{diag}\{b_{m,1}e^{j\beta_{m,1}}, b_{m,2}e^{j\beta_{m,2}}, \dots, b_{m,L}e^{j\beta_{m,L}}\} \in \mathbb{C}^{L \times L}$ and the constraints for the MS-IOS are listed as follows:

$$a_{m,l} + b_{m,l} = 1, \quad (2a)$$

$$a_{m,l}, b_{m,l} \in \{0, 1\}, \quad (2b)$$

$$0 \leq \alpha_{m,l}, \beta_{m,l} \leq 2\pi, \quad \forall l, \quad (2c)$$

where (2a) indicates that the l th element of the MS-IOS operates in either reflection or refraction mode. In addition, the signals from the transmitter and the destination are given by

$$\mathbf{x}_{DL} = \mathbf{w} s_{DL}, \quad (3)$$

$$\mathbf{x}_{UL} = \sqrt{P_d} s_{UL}, \quad (4)$$

where $\mathbf{w} \in \mathbb{C}^{M \times 1}$ is the baseband beamforming vector, P_d is the transmit power of the destination, s_{DL} and s_{UL} are the downlink and uplink transmit signals, respectively. Besides, we denote the channel coefficients between the transmit antennas and the IOS, the transmit antennas and the receive antennas, the IOS (ES-IOS/MS-IOS) and the destination, the IOS and the receive antennas, the destination and receive antennas, and between the destination itself as $\mathbf{H}_{ti} \in \mathbb{C}^{L \times M}$, $\mathbf{H}_{tr} \in \mathbb{C}^{N \times M}$, $\mathbf{h}_{id} \in \mathbb{C}^{L \times 1}$, $\mathbf{H}_{ir} \in \mathbb{C}^{L \times N}$, $\mathbf{h}_{dr} \in \mathbb{C}^{N \times 1}$ and $h_{dd} \in \mathbb{C}^{1 \times 1}$, respectively. Therefore, the received signals³ at the destination and the receiver with ES-IOS and MS-IOS are given by

$$y_{d,x} = \underbrace{\mathbf{h}_{id}^H \Phi_x \mathbf{H}_{ti} \mathbf{x}_{DL}}_{\text{desired signals}} + \underbrace{h_{dd} x_{UL}}_{\text{self interference}} + \underbrace{n_d}_{\text{noise}}, \quad (5)$$

$$y_{r,x} = \underbrace{(\mathbf{H}_{tr}^H + \mathbf{H}_{ir}^H \Theta_x \mathbf{H}_{ti}) \mathbf{x}_{DL}}_{\text{self interference}} + \underbrace{\mathbf{h}_{dr}^H x_{UL}}_{\text{desired signals}} + \underbrace{\mathbf{n}_r}_{\text{noise}}, \quad (6)$$

respectively, the first and second terms of (5) are the downlink desired signal from the transmitter and the self-interference⁴, respectively. Besides, the first and second terms of (6) are the self-interference and uplink desired signal from the destination, respectively, where $x = \{e, m\}$ denotes the case with ES-IOS and MS-IOS. $\mathbf{n}_d \sim \mathcal{CN}(0, \sigma_d^2 \mathbf{I})$ and $\mathbf{n}_r \sim \mathcal{CN}(0, \sigma_r^2 \mathbf{I})$ represent the additive Gaussian noise received at the destination and receive antennas, respectively. σ_d^2 and σ_r^2 are the noise powers at the destination and the receiver antennas, respectively. As illustrated in Fig. 1(a) and Fig. 1(b), to facilitate presentation, we characterize the positions of the transmit antennas by $(r_{l,m}, \theta_{l,m}, \phi_{l,m})$, $r_{l,m} \geq 0$, $\theta_{l,m} \in [0, \frac{\pi}{2}]$,

³We assume that the ES/MS-IOS-assisted transmitter has the knowledge of the channel state information (CSI) of the transmitter-IOS-destination link, as well as the link between transmit antennas and receive antennas. The details of the channel estimation can be found in [39, 40]. Moreover, [41] showed that the rate with estimated channels reaches that of perfect channels using the proposed PARAFAC-based method. How to perform channel estimation is out of the scope of this paper. Besides, to provide further information, we compare the imperfect CSI case as a benchmark in Section V.

⁴Since in this paper we mainly focus on the effect of the IOS at the transmitter node, the traditional SIC is assumed at the destination so that the residual SI at the destination node can be kept at the noise floor level [12, 16].

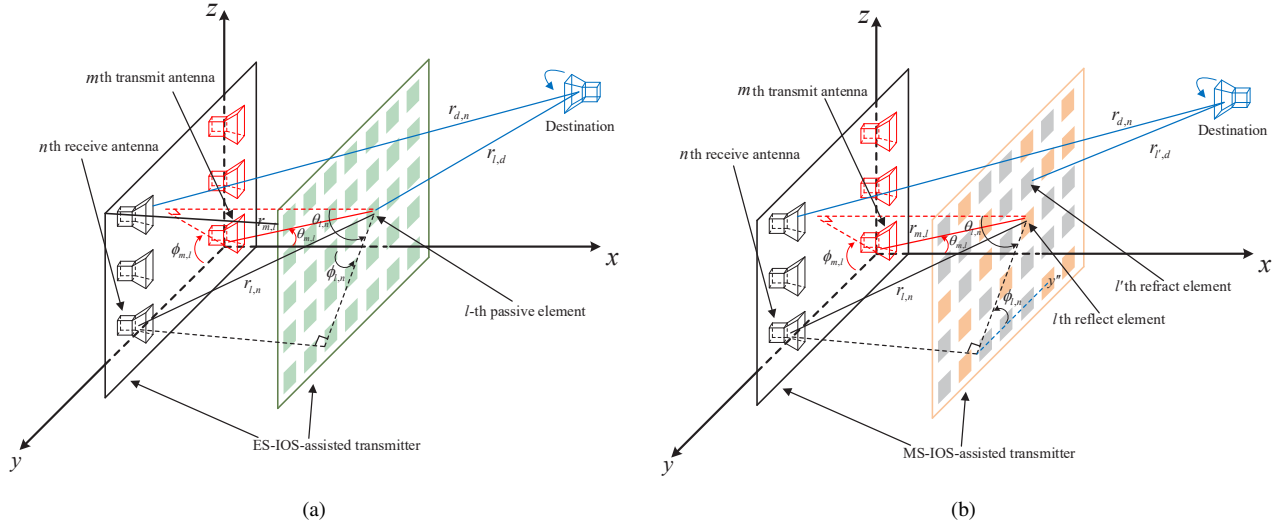


Fig. 1. (a) An ES-IOS-assisted MISO FD network. (b) An MS-IOS-assisted MISO FD network.

$\phi_{l,m} \in [0, 2\pi]$, in L different spherical coordinate systems whose respective origins are the positions of the IOS elements [42]. Here, $\theta_{l,m}$ denotes the elevation angle of the m th transmit antenna, $\phi_{l,m}$ represents the azimuth angle of the m th transmit antenna and $r_{l,m}$ is the distance between the l th IOS element and the m th transmit antenna. In a similar manner, we have the positions of the receive antennas at the elements of the IOS, the positions of the receive antennas at the transmit antennas, and the positions of the transmit antennas at the receive antennas as $(r_{l,n}, \theta_{l,n}, \phi_{l,n})$, $(r_{m,n}, \theta_{m,n}, \phi_{m,n})$ and $(r_{n,m}, \theta_{n,m}, \phi_{n,m})$, where $r_{l,n}, r_{m,n}, r_{n,m} \geq 0$, $\theta_{l,n}, \theta_{m,n}, \theta_{n,m} \in [0, \frac{\pi}{2}]$, $\phi_{l,n}, \phi_{m,n}, \phi_{n,m} \in [0, 2\pi]$. Then we can define the corresponding channel coefficients as follows:

$$\mathbf{H}_{ti} = \left[\frac{\lambda \sqrt{G^t(\theta_{l,m}, \phi_{l,m})}}{4\pi r_{l,m}} e^{-j \frac{2\pi r_{l,m}}{\lambda}} \right]_{l,m}, \quad (7)$$

$$\mathbf{H}_{tr} = \left[\frac{\lambda \sqrt{G^t(\theta_{m,n}, \phi_{m,n}) G^r(\theta_{n,m}, \phi_{n,m})}}{4\pi r_{m,n}^{\kappa/2}} \times \left(\sqrt{\frac{K}{K+1}} e^{-j \frac{2\pi r_{m,n}}{\lambda}} + \sqrt{\frac{1}{K+1}} h_{tr}^{nlos} \right) \right]_{m,n}, \quad (8)$$

$$\mathbf{h}_{dr} = \left[\frac{\lambda}{4\pi r_{d,n}^{\kappa/2}} \left(\sqrt{\frac{K}{K+1}} e^{-j \frac{2\pi r_{d,n}}{\lambda}} + \sqrt{\frac{1}{K+1}} h_{dr}^{nlos} \right) \right]_n, \quad (9)$$

$$\mathbf{h}_{id} = \left[\frac{\lambda}{4\pi r_{i,d}^{\kappa/2}} \left(\sqrt{\frac{K}{K+1}} e^{-j \frac{2\pi r_{i,d}}{\lambda}} + \sqrt{\frac{1}{K+1}} h_{id}^{nlos} \right) \right]_l, \quad (10)$$

$$\mathbf{H}_{ir} = \left[\frac{\lambda \sqrt{G^r(\theta_{l,n}, \phi_{l,n})}}{4\pi r_{l,n}} e^{-j \frac{2\pi r_{l,n}}{\lambda}} \right]_{l,n}, \quad (11)$$

where λ is the wavelength, $G^t(\theta, \phi)$ and $G^r(\theta, \phi)$ are the antenna gains at the transmit and receive antennas⁵, respectively. In addition, K and κ are Rician factor and exponent of the channels, $r_{l,d}$ and $r_{d,n}$ are the distance between the l th element

⁵The transmit and receive antenna gain models with respect to the elevation angles can be found in [42].

at the IOS and destination, and that between destination and n th receive antenna. h_{tr}^{nlos} , h_{dr}^{nlos} and h_{id}^{nlos} are the non-line-of-sight channel components, generalized using zero-mean and unit-variance circularly symmetric complex Gaussian random variables.

Then, based on (5) and (6), we can derive the data rates at the destination, the transmitter and SI power at the receive antennas for ES-IOS and MS-IOS as follows:

$$R_{d,x} = \log_2 \left(1 + \frac{\mathbf{h}_{d,x} \mathbf{w} \mathbf{w}^H \mathbf{h}_{d,x}^H}{\sigma_d^2} \right), \quad (12)$$

$$R_{r,x} = \log_2 \left(1 + \frac{\sqrt{P_d} \mathbf{h}_{dr}^H \mathbf{h}_{dr}}{\|\mathbf{H}_{r,x} \mathbf{w} \mathbf{w}^H \mathbf{H}_{r,x}^H\| + \sigma_r^2} \right), \quad (13)$$

$$P_r = \|\mathbf{H}_{r,x} \mathbf{w} \mathbf{w}^H \mathbf{H}_{r,x}^H\|, \quad (14)$$

where $\mathbf{h}_{d,x} = \mathbf{h}_{id}^H \Phi_x \mathbf{H}_{ti}$, $\mathbf{H}_{r,x} = \mathbf{H}_{tr}^H + \mathbf{H}_{ir}^H \Theta_x \mathbf{H}_{ti}$.

B. Problem formulation

In this paper, we aim to solve two optimization problems, firstly by maximizing the data rate at the destination, subject to the power consumption constraint at the transmitter, the phase shift unit modulus constraint, and the uplink rate at the receive antennas above a threshold⁶:

$$\max_{\mathbf{x}, \Phi_x, \mathbf{w}} R_{d,x} \quad (15)$$

$$\text{s.t. } \text{Tr}(\mathbf{w} \mathbf{w}^H) \leq P_{\max}, \quad (15a)$$

$$R_{r,x} \geq R_{th}^{UL}, \quad (15b)$$

$$(1a) - (1c) \text{ or } (2a) - (2c), \quad (15c)$$

where (15a) denotes the power constraint of the transmitter, P_{\max} is the maximum transmit power. In addition, (15b)

⁶In this paper, we mainly consider data rate maximization and SI power minimization with ES-IOS and MS-IOS. The balance between data rate maximization and SI power minimization can be achieved, by considering a positive weighted factor for the data rate and a negative weighted factor for the SI power, which could be considered for future work.

represents the data rate of the uplink transmission, which is above a threshold R_{th}^{UL} . Also, it is worth mentioning that the first item of (15c) is selected for the case with ES-IOS and the second item is chosen for the case with MS-IOS.

Secondly, the SI power is minimized at the transmitter, subject to the power consumption constraint at the transmitter, the phase shift unit modulus constraint and the data rate at the destination above a threshold. Accordingly, the two optimization problems are formulated as follows:

$$\min_{\Theta_x, \Phi_x, \mathbf{w}} \left\| \mathbf{H}_{r,x} \mathbf{w} \mathbf{w}^H \mathbf{H}_{r,x}^H \right\| \quad (16)$$

$$\text{s.t.} \quad \text{Tr}(\mathbf{w} \mathbf{w}^H) \leq P_{\max}, \quad (16a)$$

$$R_{d,x} \geq R_{th}^{DL}, \quad (16b)$$

$$(1a) - (1c) \text{ or } (2a) - (2c), \quad (16c)$$

where (16b) represents that the data rate of the downlink transmission at the destination above a threshold R_{th}^{DL} , and (16c) should be selected according to ES-IOS or MS-IOS mode.

III. MAXIMIZING THE DATA RATE

Given the data rate maximization problem in (15), we notice that the problem is non-convex and difficult to solve since the reflecting, refracting amplitudes/mode selection and phase shifts Θ_x , Φ_x and the beamforming vector \mathbf{w} are coupled. Especially, the mode selection optimization for MS-IOS is NP-hard, rendering the maximization problem intractable. Therefore, we propose an alternating algorithm to solve them iteratively.

A. Optimizing beamforming vector \mathbf{w} for given Θ_x and Φ_x

Firstly, with given reflecting and refracting amplitudes and phase shifts Θ_x and Φ_x for ES-IOS and MS-IOS, the beamforming vector \mathbf{w} optimization problem for maximizing the data rate at the destination can be reformulated as follows:

$$\max_{\mathbf{w}} \log_2 \left(1 + \frac{\mathbf{h}_{d,x} \mathbf{w} \mathbf{w}^H \mathbf{h}_{d,x}^H}{\sigma_d^2} \right) \quad (17)$$

$$\text{s.t.} \quad \text{Tr}(\mathbf{w} \mathbf{w}^H) \leq P_{\max}, \quad (17a)$$

$$\log_2 \left(1 + \frac{\sqrt{P_d} \mathbf{h}_{dr}^H \mathbf{h}_{dr}}{\|\mathbf{H}_{r,x} \mathbf{w} \mathbf{w}^H \mathbf{H}_{r,x}^H\| + \sigma_r^2} \right) \geq R_{th}^{UL}, \quad (17b)$$

which is equivalent to the following problem:

$$\max_{\mathbf{w}} \mathbf{w}^H \mathbf{h}_{d,x}^H \mathbf{h}_{d,x} \mathbf{w} \quad (18)$$

$$\text{s.t.} \quad \text{Tr}(\mathbf{w} \mathbf{w}^H) \leq P_{\max}, \quad (18a)$$

$$\text{Tr}(\mathbf{w}^H \mathbf{H}_{r,x}^H \mathbf{H}_{r,x} \mathbf{w}) \leq \frac{\sqrt{P_d} \mathbf{h}_{dr}^H \mathbf{h}_{dr}}{2^{R_{th}^{UL}} - 1}, \quad (18b)$$

however, this problem is still non-convex due to the non-concavity of the objective function. Thus by applying the first-order Taylor expansion to (18), the objective function can be convexified as [24]:

$$\mathbf{w}^H \mathbf{h}_{d,x}^H \mathbf{h}_{d,x} \mathbf{w} \geq 2 \text{Re} \left\{ \mathbf{w}^H \mathbf{h}_{d,x}^H \mathbf{h}_{d,x} \tilde{\mathbf{w}} \right\} - \tilde{\mathbf{w}}^H \mathbf{h}_{d,x}^H \mathbf{h}_{d,x} \tilde{\mathbf{w}}, \quad (19)$$

where $\tilde{\mathbf{w}}$ is the beamforming vector value of the last iteration. Therefore, the beamforming vector optimization problem can be formulated as follows:

$$\max_{\mathbf{w}} \text{Re} \left\{ \mathbf{w}^H \mathbf{h}_{d,x}^H \mathbf{h}_{d,x} \tilde{\mathbf{w}} \right\} \quad (20)$$

$$\text{s.t.} \quad \text{Tr}(\mathbf{w} \mathbf{w}^H) \leq P_{\max}, \quad (20a)$$

$$\text{Tr}(\mathbf{w}^H \mathbf{H}_{r,x}^H \mathbf{H}_{r,x} \mathbf{w}) \leq \frac{\sqrt{P_d} \mathbf{h}_{dr}^H \mathbf{h}_{dr}}{2^{R_{th}^{UL}} - 1}, \quad (20b)$$

which is a QCQP problem and can be solved by convex optimization tools such as CVX.

B. Optimizing reflecting and refracting amplitudes/mode selection and phase shifts Θ_x and Φ_x for given \mathbf{w}

Secondly, since the binary optimization in mode selection for the case with MS-IOS is NP-hard, we classify the data rate maximization problem into the two cases for a given beamforming vector \mathbf{w} , according to the type of IOS.

a) Optimizing reflecting and refracting amplitudes and phase shifts Θ_e and Φ_e for ES-IOS

For a given beamforming vector \mathbf{w} , the data rate maximization problem with the ES-IOS can be reformulated as follows:

$$\max_{\Theta_e, \Phi_e} \mathbf{h}_{id}^H \Phi_e \mathbf{H}_{ti} \mathbf{w} \mathbf{w}^H \mathbf{H}_{ti}^H \Phi_e^H \mathbf{h}_{id} \quad (21)$$

$$\text{Tr} \left(\left(\mathbf{H}_{tr}^H + \mathbf{H}_{ir}^H \Theta_e \mathbf{H}_{ti} \right) \mathbf{w} \mathbf{w}^H \left(\mathbf{H}_{tr}^H + \mathbf{H}_{ti}^H \Theta_e^H \mathbf{H}_{ir} \right) \right) \quad (21a)$$

$$\text{s.t.} \quad \leq \frac{\sqrt{P_d} \mathbf{h}_{dr}^H \mathbf{h}_{dr}}{2^{R_{th}^{UL}} - 1}, \quad (21a)$$

$$a_{e,l}^2 + b_{e,l}^2 \leq 1, \quad (21b)$$

$$0 \leq a_{e,l}, b_{e,l} \leq 1, \quad (21c)$$

$$0 \leq \alpha_{e,l}, \beta_{e,l} \leq 2\pi, \quad \forall l, \quad (21d)$$

which can be reformulated as

$$\max_{\Theta_e, \Phi_e} \text{Tr} \left(\Phi_e^H \mathbf{X}_{e,1} \Phi_e \mathbf{Y}_{e,1} \right) \quad (22)$$

$$\text{Tr} \left(\Theta_e^H \mathbf{X}_{e,2} \Theta_e \mathbf{Y}_{e,2} \right) + \text{Tr} \left(\Theta_e \mathbf{Z}_{e,2} \right) \quad (22a)$$

$$\text{s.t.} \quad + \text{Tr} \left(\Theta_e^H \mathbf{Z}_{e,2} \right) + d_{e,2} \leq \frac{\sqrt{P_d} \mathbf{h}_{dr}^H \mathbf{h}_{dr}}{2^{R_{th}^{UL}} - 1}, \quad (22a)$$

$$a_{e,l}^2 + b_{e,l}^2 \leq 1, \quad (22b)$$

$$0 \leq a_{e,l}, b_{e,l} \leq 1, \quad (22c)$$

$$0 \leq \alpha_{e,l}, \beta_{e,l} \leq 2\pi, \quad \forall l, \quad (22d)$$

where

$$\mathbf{X}_{e,1} = \mathbf{h}_{id} \mathbf{h}_{id}^H, \quad \mathbf{X}_{e,2} = \mathbf{H}_{ir} \mathbf{H}_{ir}^H, \quad d_{e,2} = \text{Tr} \left(\mathbf{H}_{tr}^H \mathbf{w} \mathbf{w}^H \mathbf{H}_{tr} \right),$$

$$\mathbf{Y}_{e,1} = \mathbf{Y}_{e,2} = \mathbf{H}_{ti} \mathbf{w} \mathbf{w}^H \mathbf{H}_{ti}^H, \quad \mathbf{Z}_{e,2} = \mathbf{H}_{ti} \mathbf{w} \mathbf{w}^H \mathbf{H}_{tr} \mathbf{H}_{tr}^H.$$

However, this problem is still not convex due to the objective function (22) and constraints (22b)-(22d). By introducing new variables $\alpha_e = [a_{e,1} e^{j\alpha_{e,1}}, a_{e,2} e^{j\alpha_{e,2}}, \dots, a_{e,L} e^{j\alpha_{e,L}}] \in \mathbb{C}^{L \times 1}$ and $\beta_e = [b_{e,1} e^{j\beta_{e,1}}, b_{e,2} e^{j\beta_{e,2}}, \dots, b_{e,L} e^{j\beta_{e,L}}] \in \mathbb{C}^{L \times 1}$, we can reformulate the constraint (22b)-(22d) as follows:

$$\text{diag} \left\{ \alpha_e \alpha_e^H + \beta_e \beta_e^H \right\} \leq \mathbf{1}_L, \quad (23)$$

Algorithm 1 Gaussian randomization procedure

1. Set a number of randomizations G , given the SDR solution \mathbf{X} .
2. Generate $\xi_g \sim \mathcal{N}(\mathbf{0}, \mathbf{X})$, $g = 1, 2, \dots, G$ and construct a feasible point $\tilde{\mathbf{x}}_g = \text{sgn}(\xi_g)$.
3. Determine $g^* = \arg \max_{g=1, \dots, G} \text{Tr}(\Xi'_{m,1} \tilde{\mathbf{x}}_g \tilde{\mathbf{x}}_g^T)$ and $[\mathbf{x}_{g^*}]_{L+1} = 1$ for the data rate maximization problem, $g^* = \arg \min_{g=1, \dots, G} \text{Tr}(\Xi'_{m,2} \tilde{\mathbf{x}}_g \tilde{\mathbf{x}}_g^T)$ and $[\mathbf{x}_{g^*}]_{L+1} = 1$ for the SI power minimization problem.
4. Set $\mathbf{b} = [\mathbf{x}_{g^*}]_{1:L}$, calculate $\mathbf{a}_m = \frac{\mathbf{b} + \mathbf{1}_L}{2}$, and output $\mathbf{A}_m = \text{diag}\{\mathbf{a}_m\}$.

which is now convex with respect to α_e and β_e . In addition, according to the matrix properties in [43, Eq. (1.10.6)], we have $\text{Tr}(\Phi_e^H \mathbf{X}_{e,1} \Phi_e \mathbf{Y}_{e,1}) = \beta_e^H \Xi_{e,1} \beta_e$ and

$$\begin{aligned} & \text{Tr}(\Theta_e^H \mathbf{X}_{e,2} \Theta_e \mathbf{Y}_{e,2}) + \text{Tr}(\Theta_e \mathbf{Z}_{e,2}) + \text{Tr}(\Theta_e^H \mathbf{Z}_{e,2}^H) + d_{e,2} \\ &= \alpha_e^H \Xi_{e,2} \alpha_e + \mathbf{z}_{e,2}^H \alpha_e^* + \alpha_e^T \mathbf{z}_{e,2} + d_{e,2}, \end{aligned} \quad (24)$$

where $\Xi_{e,1} = \mathbf{X}_{e,1} \odot \mathbf{Y}_{e,1}$, $\Xi_{e,2} = \mathbf{X}_{e,2} \odot \mathbf{Y}_{e,2}$ and $\mathbf{z}_{e,2} = \text{diag}\{\mathbf{Z}_{e,2}\}$. Therefore, the reflecting and refracting phase shifts optimization problem for maximizing the data rate can be reformulated as follows:

$$\max_{\alpha_e, \beta_e} \beta_e^H \Xi_{e,1} \beta_e \quad (25)$$

$$\text{s.t. } \text{diag}\{\alpha_e \alpha_e^H + \beta_e \beta_e^H\} \leq \mathbf{1}_L, \quad (25a)$$

$$\alpha_e^H \Xi_{e,2} \alpha_e + \mathbf{z}_{e,2}^H \alpha_e^* + \alpha_e^T \mathbf{z}_{e,2} + d_{e,2} \leq \frac{\sqrt{P_d} \mathbf{h}_{dr}^H \mathbf{h}_{dr}}{2^{R_{th}^{UL}} - 1}, \quad (25b)$$

so far, (25) is the only obstacle for this optimization, which can be approximated via the first-order Taylor expansion as follows:

$$\beta_e^H \Xi_{e,1} \beta_s \geq 2 \text{Re}\{\beta_e^H \Xi_{e,1} \tilde{\beta}_e\} - \tilde{\beta}_e^H \Xi_{e,1} \tilde{\beta}_e, \quad (26)$$

where $\tilde{\beta}_e$ is the refracting phase shifts derived at the last iteration, therefore, the reflecting and refracting phase shifts optimization can be rewritten as follows:

$$\max_{\alpha_e, \beta_e} \text{Re}\{\beta_e^H \Xi_{e,1} \tilde{\beta}_e\} \quad (27)$$

$$\text{s.t. } \text{diag}\{\alpha_e \alpha_e^H + \beta_e \beta_e^H\} \leq \mathbf{1}_L, \quad (27a)$$

$$\alpha_e^H \Xi_{e,2} \alpha_e + \mathbf{z}_{e,2}^H \alpha_e^* + \alpha_e^T \mathbf{z}_{e,2} + d_{e,2} \leq \frac{\sqrt{P_d} \mathbf{h}_{dr}^H \mathbf{h}_{dr}}{2^{R_{th}^{UL}} - 1}, \quad (27b)$$

which now is a convex problem with convex constraints, and can be solved by CVX using QCQP. Therefore, the joint amplitudes and phase shifts of the ES-IOS are solved. In addition, the overall algorithm for maximizing the data rate for the ES-IOS is summarized in Algorithm 1.

b) *Optimizing reflecting and refracting phase shifts Θ'_m and Φ'_m for MS-IOS*

In the MS-IOS case, with a given beamforming vector \mathbf{w} , we reformulate the rate maximization problem as follows:

$$\max_{\Theta'_m, \Phi'_m} \mathbf{h}_{id}^H \Phi'_m \mathbf{H}_{ti} \mathbf{w} \mathbf{w}^H \mathbf{H}_{ti}^H \Phi'_m \mathbf{h}_{id} \quad (28)$$

$$\begin{aligned} & \text{Tr}\left(\left(\mathbf{H}_{tr}^H + \mathbf{H}_{ir}^H \Theta'_m \mathbf{H}_{ti}\right) \mathbf{w} \mathbf{w}^H \left(\mathbf{H}_{tr}^H + \mathbf{H}_{ti}^H \Theta'_m \mathbf{H}_{ir}\right)\right) \\ & \text{s.t. } \leq \frac{\sqrt{P_d} \mathbf{h}_{dr}^H \mathbf{h}_{dr}}{2^{R_{th}^{UL}} - 1}, \end{aligned} \quad (28a)$$

$$a_{m,l} + b_{m,l} = 1, \quad (28b)$$

$$a_{m,l}, b_{m,l} \in \{0, 1\}, \quad (28c)$$

$$0 \leq \alpha_{m,l}, \beta_{m,l} \leq 2\pi, \quad \forall l, \quad (28d)$$

however, this problem is non-convex since the binary variables are contained in the coefficient matrices. To tackle this problem, we further divide the problem into two sub-problems.

Firstly, we reconstruct the phase shifts coefficient matrices as $\Theta'_m = \mathbf{A}_m \Theta'_m$ and $\Phi'_m = \mathbf{B}_m \Phi'_m$, where $\mathbf{A}_m = \text{diag}\{a_{m,1}, a_{m,2}, \dots, a_{m,L}\} \in \mathbb{C}^{L \times L}$ and $\mathbf{B}_m = \text{diag}\{b_{m,1}, b_{m,2}, \dots, b_{m,L}\} \in \mathbb{C}^{L \times L}$ indicate the elements for reflecting and refracting. $\Theta'_m = \text{diag}\{e^{j\alpha_{m,1}}, e^{j\alpha_{m,2}}, \dots, e^{j\alpha_{m,L}}\} \in \mathbb{C}^{L \times L}$ and $\Phi'_m = \text{diag}\{e^{j\beta_{m,1}}, e^{j\beta_{m,2}}, \dots, e^{j\beta_{m,L}}\} \in \mathbb{C}^{L \times L}$ are the reflecting and refracting phase shifts matrices, respectively. Thereby, the channels can be reformulated as follows:

$$\mathbf{h}_{d,m} = \mathbf{h}_{id}^H (\mathbf{I} - \mathbf{A}_m) \Phi'_m \mathbf{H}_{ti}, \quad (29)$$

$$\mathbf{H}_{r,m} = \mathbf{H}_{tr}^H + \mathbf{H}_{ir}^H \mathbf{A}_m \Phi'_m \mathbf{H}_{ti}, \quad (30)$$

then the problem with fixed mode selection matrix \mathbf{A}_m and \mathbf{B}_m can be reformulated as follows:

$$\max_{\Theta'_m, \Phi'_m} \mathbf{h}_{id}^H (\mathbf{I} - \mathbf{A}_m) \Phi'_m \mathbf{H}_{ti} \mathbf{w} \mathbf{w}^H \mathbf{H}_{ti}^H \Phi'^H (\mathbf{I} - \mathbf{A}_m)^H \mathbf{h}_{id} \quad (31)$$

$$\begin{aligned} & \text{Tr}\left(\left(\mathbf{H}_{tr}^H + \mathbf{H}_{ir}^H \mathbf{A}_m \Theta'_m \mathbf{H}_{ti}\right) \mathbf{w} \mathbf{w}^H \left(\mathbf{H}_{tr}^H + \mathbf{H}_{ti}^H \Theta'_m \mathbf{A}_m \mathbf{H}_{ir}\right)\right) \\ & \text{s.t. } \leq \frac{\sqrt{P_d} \mathbf{h}_{dr}^H \mathbf{h}_{dr}}{2^{R_{th}^{UL}} - 1}, \end{aligned} \quad (31a)$$

$$0 \leq \alpha_{m,l}, \beta_{m,l} \leq 2\pi, \quad \forall l. \quad (31b)$$

Note that by introducing $\alpha_m = [e^{j\alpha_{m,1}}, e^{j\alpha_{m,2}}, \dots, e^{j\alpha_{m,L}}] \in \mathbb{C}^{L \times 1}$ and $\beta_m = [e^{j\beta_{m,1}}, e^{j\beta_{m,2}}, \dots, e^{j\beta_{m,L}}] \in \mathbb{C}^{L \times 1}$, the constraint (31b) can be reformulated as

$$\text{diag}\{\alpha_m \alpha_m^H\} = \mathbf{1}_L, \quad (32)$$

$$\text{diag}\{\beta_m \beta_m^H\} = \mathbf{1}_L, \quad (33)$$

and the problem can be reformulated as

$$\max_{\alpha_m, \beta_m} \beta_m^H \Xi_{m,1} \beta_m \quad (34)$$

$$\text{s.t. } \alpha_m^H \Xi_{m,2} \alpha_m + \mathbf{z}_{m,2}^H \alpha_m^* + \alpha_m^T \mathbf{z}_{m,2} + d_{m,2} \leq \frac{\sqrt{P_d} \mathbf{h}_{dr}^H \mathbf{h}_{dr}}{2^{R_{th}^{UL}} - 1}, \quad (34a)$$

$$\text{diag}\{\alpha_m \alpha_m^H\} = \mathbf{1}_L, \quad (34b)$$

$$\text{diag}\{\beta_m \beta_m^H\} = \mathbf{1}_L, \quad (34c)$$

where

$$\Xi_{m,1} = \mathbf{X}_{m,1} \odot \mathbf{Y}_{m,1}, \quad \Xi_{m,2} = \mathbf{X}_{m,2} \odot \mathbf{Y}_{m,2},$$

$$\begin{aligned} \mathbf{X}_{m,1} &= (\mathbf{I} - \mathbf{A}_m)^H \mathbf{h}_{id} \mathbf{h}_{id}^H (\mathbf{I} - \mathbf{A}_m), \quad \mathbf{X}_{m,2} = \mathbf{A}_o^H \mathbf{H}_{ir} \mathbf{H}_{ir}^H \mathbf{A}_m, \\ \mathbf{Y}_{m,1} &= \mathbf{H}_{ti} \mathbf{H}_{ti}^H, \quad \mathbf{Y}_{m,2} = \mathbf{H}_{ti} \mathbf{w} \mathbf{w}^H \mathbf{H}_{ti}^H, \\ \mathbf{Z}_{m,2} &= \mathbf{H}_{ti} \mathbf{w} \mathbf{w}^H \mathbf{H}_{tr} \mathbf{H}_{tr}^H \mathbf{A}_m, \quad d_{m,2} = \text{Tr} \left(\mathbf{H}_{tr}^H \mathbf{w} \mathbf{w}^H \mathbf{H}_{tr} \right), \end{aligned}$$

and $\mathbf{z}_{m,2} = \text{diag}\{\mathbf{Z}_{m,2}\}$, however, this problem is non-convex due to (34), (34b) and (34c). By applying the first-order Taylor expansion to (34), and relaxation to (34b) and (34c), the problem can be transformed as follows:

$$\max_{\alpha_m, \beta_m} \text{Re} \left\{ \beta_m^H \Xi_m,1 \tilde{\beta}_m \right\} \quad (35)$$

$$\text{s.t. } \alpha_m^H \Xi_m,2 \alpha_m + \mathbf{z}_{m,2}^H \alpha_m^* + \alpha_m^T \mathbf{z}_{m,2} + d_{m,2} \leq \frac{\sqrt{P_d} \mathbf{h}_{dr}^H \mathbf{h}_{dr}}{2^{R_{th}^{UL}} - 1}, \quad (35a)$$

$$\text{diag} \left\{ \alpha_m \alpha_m^H \right\} \leq \mathbf{1}_L, \quad (35b)$$

$$\text{diag} \left\{ \beta_m \beta_m^H \right\} \leq \mathbf{1}_L, \quad (35c)$$

where $\tilde{\beta}_o$ is the value at the last iteration, now this problem can be solved. In the following subsection, the mode selection for the case with MS-IOs will be discussed.

C. Optimizing mode selection \mathbf{A}_m with given \mathbf{w} , Θ'_m and Φ'_m for MS-IOs

In this subsection, we aim to optimize \mathbf{A}_m with given phase shifts and beamforming vector, for the case with MS-IOs. The problem is formulated as follows:

$$\max_{\mathbf{A}_m} \mathbf{h}_{id}^H (\mathbf{I} - \mathbf{A}_m) \Phi'_m \mathbf{H}_{ti} \mathbf{w} \mathbf{w}^H \mathbf{H}_{ti}^H \Phi_m^H (\mathbf{I} - \mathbf{A}_m)^H \mathbf{h}_{id} \quad (36)$$

$$\text{s.t. } \text{Tr} \left(\left(\mathbf{H}_{tr}^H + \mathbf{H}_{ir}^H \mathbf{A}_m \Theta_m \mathbf{H}_{ir} \right) \mathbf{w} \mathbf{w}^H \left(\mathbf{H}_{tr} + \mathbf{H}_{tr} \Theta_m^H \mathbf{A}_m^H \mathbf{H}_{tr} \right) \right) \leq \frac{\sqrt{P_d} \mathbf{h}_{dr}^H \mathbf{h}_{dr}}{2^{R_{th}^{UL}} - 1}, \quad (36a)$$

$$a_{m,l} + b_{m,l} = 1, \quad (36b)$$

$$a_{m,l}, b_{m,l} \in \{0, 1\}, \quad (36c)$$

however, this problem is difficult to tackle due to the binary variables. Firstly, we need to reconstruct the problem, by introducing a vector $\mathbf{a}_m = [a_{m,1}, a_{m,2}, \dots, a_{m,L}] \in \mathbb{C}^{L \times 1}$, we can rewrite the problem as follows:

$$\max_{\mathbf{a}_m} \mathbf{a}_m^T \Xi_m,1 \mathbf{a}_m - 2 \text{Re} \left\{ \mathbf{a}_m^T \mathbf{w}_{m,1} \right\} + d_{m,1} \quad (37)$$

$$\text{s.t. } \mathbf{a}_m^T \Xi_m,2 \mathbf{a}_m + 2 \text{Re} \left\{ \mathbf{a}_m^T \mathbf{w}_{m,2} \right\} + d_{m,2} \leq \frac{\sqrt{P_d} \mathbf{h}_{dr}^H \mathbf{h}_{dr}}{2^{R_{th}^{UL}} - 1}, \quad (37a)$$

$$a_{m,l} \in \{0, 1\}, \quad (37c)$$

where

$$\Xi_m,1 = \mathbf{U}_{m,1} \odot \mathbf{V}_{m,1}, \quad \Xi_m,2 = \mathbf{U}_{m,2} \odot \mathbf{V}_{m,2},$$

$$\mathbf{U}_{m,1} = \mathbf{h}_{id} \mathbf{h}_{id}^H, \quad \mathbf{V}_{m,1} = \Phi'_m \mathbf{H}_{ti} \mathbf{w} \mathbf{w}^H \mathbf{H}_{ti}^H \Phi_m^H,$$

$$\mathbf{U}_{m,2} = \mathbf{H}_{ir} \mathbf{H}_{ir}^H, \quad \mathbf{V}_{m,2} = \Theta'_m \mathbf{H}_{tr} \mathbf{w} \mathbf{w}^H \mathbf{H}_{tr}^H \Theta_m^H,$$

$$\mathbf{W}_{m,1} = \text{diag} \left\{ \mathbf{h}_{id}^H \right\} \Phi'_m \mathbf{H}_{ti} \mathbf{w} \mathbf{w}^H \mathbf{H}_{ti}^H \Phi_m^H \mathbf{h}_{id},$$

$$\mathbf{W}_{m,2} = \Theta'_m \mathbf{H}_{tr} \mathbf{w} \mathbf{w}^H \mathbf{H}_{tr}^H \mathbf{H}_{ir}^H,$$

Algorithm 2 Data rate maximizations for both ES-IOs and MS-IOs

Initialize the beamforming vector \mathbf{w}^0 , the reflecting, refracting amplitudes and phase shifts Θ_e^0 , Φ_e^0 of the ES-IOs, the phase shifts matrix of MS-IOs Θ_m^0 , Φ_m^0 , as well as the mode selection matrix of the MS-IOs \mathbf{A}_m^0 , compute $R_{d,e}(\mathbf{w}^0, \Theta_e^0, \Phi_e^0)$ and $R_{d,m}(\mathbf{w}^0, \Theta_m^0, \Phi_m^0, \mathbf{A}_m^0)$, respectively. Set $t = 0$ and the accuracy for iteration ε_1 .

repeat

1. Given \mathbf{w}^t , \mathbf{A}_m^0 , Θ_e^t , Φ_e^t , Θ_m^t and Φ_m^t , compute the data rates as $R_{d,e}(\mathbf{w}^t, \Theta_e^t, \Phi_e^t)$ and $R_{d,m}(\mathbf{w}^t, \Theta_m^t, \Phi_m^t, \mathbf{A}_m^t)$, respectively.

2. Given Θ_e^t , Φ_e^t for the case with ES-IOs and given \mathbf{A}_m^t , Θ_m^t and Φ_m^t for the case with MS-IOs, optimize \mathbf{w}^{t+1} by solving problem (20).

3. Given \mathbf{w}^{t+1} , optimize Θ_e^{t+1} and Φ_e^{t+1} by solving problem (27) for the ES-IOs. As for the MS-IOs, optimize Θ_m^{t+1} and Φ_m^{t+1} with given \mathbf{w}^{t+1} and \mathbf{A}_m^t for the case with MS-IOs, by solving problem (35).

4. By solving (42) for the case with MS-IOs, optimize \mathbf{X} given \mathbf{w}^{t+1} , Θ_m^{t+1} and Φ_m^{t+1} .

5. For the case with MS-IOs, retrieve \mathbf{A}_m^{t+1} from \mathbf{X} using Gaussian randomization procedure.

6. Compute the data rates $R_{d,e}(\mathbf{w}^{t+1}, \Theta_e^{t+1}, \Phi_e^{t+1})$ and $R_{d,m}(\mathbf{w}^{t+1}, \Theta_m^{t+1}, \Phi_m^{t+1}, \mathbf{A}_m^t)$ for both the IOs.

7. Set $t = t + 1$.

until $\frac{|R_{d,e}(\mathbf{w}^{t+1}, \Theta_e^{t+1}, \Phi_e^{t+1}) - R_{d,e}(\mathbf{w}^t, \Theta_e^t, \Phi_e^t)|}{R_{d,e}(\mathbf{w}^{t+1}, \Theta_e^{t+1}, \Phi_e^{t+1})} \leq \varepsilon_1$ or $\frac{|R_{d,m}(\mathbf{w}^{t+1}, \Theta_m^{t+1}, \Phi_m^{t+1}, \mathbf{A}_m^{t+1}) - R_{d,m}(\mathbf{w}^t, \Theta_m^t, \Phi_m^t, \mathbf{A}_m^t)|}{R_{d,m}(\mathbf{w}^{t+1}, \Theta_m^{t+1}, \Phi_m^{t+1}, \mathbf{A}_m^{t+1})} \leq \varepsilon_1$.

$$d_{m,1} = \mathbf{h}_{id}^H \Phi'_m \mathbf{H}_{ti} \mathbf{w} \mathbf{w}^H \mathbf{H}_{ti}^H \Phi_m^H \mathbf{h}_{id}, \quad d_{m,2} = \text{Tr} \left(\mathbf{H}_{tr}^H \mathbf{w} \mathbf{w}^H \mathbf{H}_{tr} \right).$$

However, (37) is still not convex due to the binary variables. By reconstructing the expressions $\mathbf{a}_m^T \Xi_m,1 \mathbf{a}_m = \sum_{l_1=1}^L \sum_{l_2=1}^L [\Xi_m,1]_{l_1, l_2} a_{l_1} a_{l_2}$, and $\text{Re} \left\{ \mathbf{a}_m^T \mathbf{w}_{m,1} \right\} = \sum_{l_1=1}^L a_{l_1} [\text{Re} \left\{ \mathbf{w}_{m,1} \right\}]_{l_1}$. In addition, by introducing slack variables $\mathbf{S}_m = \{s_{l_1, l_2} | l_1, l_2 = 1, 2, \dots, L\} \in \mathbb{C}^{L \times L}$ we can reformulate the problem as follows:

$$\max_{\mathbf{a}_m, \mathbf{S}_m} \sum_{l_1=1}^L \sum_{l_2=1}^L [\Xi_m,1]_{l_1, l_2} s_{l_1, l_2} - 2a_{l_1} \sum_{l_1=1}^L [\text{Re} \left\{ \mathbf{w}_{m,1} \right\}]_{l_1} \quad (38)$$

$$\text{s.t. } \sum_{l_1=1}^L \sum_{l_2=1}^L [\Xi_m,2]_{l_1, l_2} s_{l_1, l_2} + 2a_{l_1} \sum_{l_1=1}^L [\text{Re} \left\{ \mathbf{w}_{m,2} \right\}]_{l_1} \quad (38a)$$

$$+ d_{m,2} \leq \frac{\sqrt{P_d} \mathbf{h}_{dr}^H \mathbf{h}_{dr}}{2^{R_{th}^{UL}} - 1},$$

$$a_{m,l} \in \{0, 1\}, \quad (38b)$$

$$s_{l_1, l_2} \leq a_{l_1}, \quad (38c)$$

$$s_{l_1, l_2} \leq a_{l_2}, \quad (38d)$$

$$s_{l_1, l_2} \geq a_{l_1} + a_{l_2} - 1, \quad (38e)$$

this problem can be solved by CVX, however, is NP-hard [44] thus this problem is intractable for a large L .

Thus, we transform the above problem using the SDR method. By introducing a new binary variable $\mathbf{b} = 2\mathbf{a}_m - \mathbf{1}_L \in \mathbb{R}^{L \times 1}$, where $\mathbf{b} = [b_1, b_2, \dots, b_L]^T$ and $b_l \in \{-1, 1\}$, then the objective function of the rate maximization problem is given by

$$\frac{1}{4} \left(\text{Tr}(\Xi_m,1 \mathbf{B}) + 2 \text{Re} \left\{ \mathbf{h}^T \mathbf{b} \right\} \right) + c_{m,1}, \quad (39)$$

where $\mathbf{B} = \mathbf{b}\mathbf{b}^T$. Thereby, by introducing another binary slack variable $\mathbf{x} = [\mathbf{b}; \mathbf{1}] \in \mathbb{R}^{(L+1) \times 1}$, we can reconstruct the objective function and the SI power as

$$\frac{1}{4} \text{Tr}(\Xi'_{m,1} \mathbf{X}) + c_{m,1}, \quad (40)$$

$$\frac{1}{4} \text{Tr}(\Xi'_{m,2} \mathbf{X}) + c_{m,2}, \quad (41)$$

respectively. The derivation is given in Appendix A.

Thus, the problem can be transformed as follows:

$$\max_{\mathbf{X}} \frac{1}{4} \text{Tr}(\Xi'_{m,1} \mathbf{X}) + c_{m,1} \quad (42)$$

$$\text{s.t.} \quad \frac{1}{4} \text{Tr}(\Xi'_{m,2} \mathbf{X}) + c_{m,2} \leq \frac{\sqrt{P_d} \mathbf{h}_{dr}^H \mathbf{h}_{dr}}{2^{R_{th}^{UL}} - 1}, \quad (42a)$$

$$\text{diag}\{\mathbf{X}\} = \mathbf{1}_{L+1}, \quad (42b)$$

$$\text{Rank}(\mathbf{X}) = 1, \quad (42c)$$

however, the rank-one constraint renders the problem infeasible, thus by dropping this constraint, we can optimize the problem by utilizing the SDR method. Then using the Gaussian randomization procedure, we can extract \mathbf{a}_m from \mathbf{X} , the details of the Gaussian randomization procedure is provided in Algorithm 1.

D. Overall Algorithm, convergence and complexity analysis

In a nutshell, the overall alternative optimization algorithm for maximizing the data rate is provided in Algorithm 2. The QCQP method is applied to solve the beamforming vector, the reflecting, refracting amplitudes and phase shifts optimization for the case with the ES-IOs and phase shifts optimization for the case with the MS-IOs. Furthermore, the SDR method and Gaussian randomization procedure are exploited for solving the element mode selection for MS-IOs. Every step in Algorithm 2 guarantees the objective function increases monotonically, that is, $R_{d,x}(\mathbf{w}^{t+1}, \Theta_x^{t+1}, \Phi_x^{t+1}) > R_{d,x}(\mathbf{w}^t, \Theta_x^t, \Phi_x^t) > \dots > R_{d,x}(\mathbf{w}^0, \Theta_x^0, \Phi_x^0)$, therefore, the proposed algorithm's convergence is guaranteed. It is worth pointing out that the complexity of the QCQP method for beamforming optimization is on the order of $\mathcal{O}(M^3)$ [45], and the computational complexities of the QCQP method for optimizing phase shifts matrices for both the ES-IOs and MS-IOs are $\mathcal{O}(L^3)$. In addition, the computational complexities of the SDR method and Gaussian randomization procedure for the mode selection optimization with the MS-IOs are $\mathcal{O}(L^{3.5})$ [46] and $\mathcal{O}(G)$, respectively. Therefore, the overall complexity order of the proposed system amounts to $\mathcal{O}(N_{ite} \times \max\{M^3, L^3\})$ and $\mathcal{O}(N_{ite} \times \max\{M^3, L^{3.5}, G\})$, respectively, where N_{ite} is the number of optimization iterations and G is the number for randomizations.

IV. MINIMIZING THE SI POWER

To minimize the SI power, we notice that the problem is difficult to solve since the reflecting, refracting amplitudes/mode selection and phase shifts Θ_x , Φ_x and the beamforming vector \mathbf{w} are coupled. Therefore, we propose an alternating algorithm to solve them iteratively.

A. Optimizing beamforming vector \mathbf{w} for given Θ_x and Φ_x

Firstly, with given reflecting, refracting amplitudes/mode selection and phase shifts Θ_x and Φ_x for ES-IOs and MS-IOs, the SI power minimization problem can be reformulated as follows:

$$\min_{\mathbf{w}} \left\| \mathbf{H}_{r,x} \mathbf{w} \mathbf{w}^H \mathbf{H}_{r,x}^H \right\| \quad (43)$$

$$\text{s.t.} \quad \text{Tr}(\mathbf{w} \mathbf{w}^H) \leq P_{\max}, \quad (43a)$$

$$\log_2 \left(1 + \frac{\mathbf{h}_{d,x} \mathbf{w} \mathbf{w}^H \mathbf{h}_{d,x}^H}{\sigma_d^2} \right) \geq R_{th}^{DL}, \quad (43b)$$

which can be rewritten as follows:

$$\min_{\mathbf{w}} \mathbf{w}^H \mathbf{H}_{r,x}^H \mathbf{H}_{r,x} \mathbf{w} \quad (44)$$

$$\text{s.t.} \quad \mathbf{w}^H \mathbf{w} \leq P_{\max}, \quad (44a)$$

$$\mathbf{w}^H \mathbf{h}_{d,x}^H \mathbf{h}_{d,x} \mathbf{w} \geq \left(2^{R_{th}^{DL}} - 1 \right) \sigma_d^2. \quad (44b)$$

We notice that constraint (44b) renders this problem non-convex, by using the first-order Taylor expansion, this problem can be reformulated as a convex optimization problem:

$$\min_{\mathbf{w}} \mathbf{w}^H \mathbf{H}_{r,x}^H \mathbf{H}_{r,x} \mathbf{w} \quad (45)$$

$$\text{s.t.} \quad \mathbf{w}^H \mathbf{w} \leq P_{\max}, \quad (45a)$$

$$2 \text{Re} \left\{ \mathbf{w}^H \mathbf{h}_d^H \mathbf{h}_d \tilde{\mathbf{w}} \right\} \geq \tilde{\mathbf{w}}^H \mathbf{h}_{d,x}^H \mathbf{h}_{d,x} \tilde{\mathbf{w}} + \left(2^{R_{th}^{DL}} - 1 \right) \sigma_d^2, \quad (45b)$$

which is a QCQP problem and can be solved.

B. Optimizing reflecting and refracting amplitudes/mode selection and phase shifts Θ_x and Φ_x for given \mathbf{w}

Firstly, we aim to optimize reflecting, refracting amplitudes/mode selection and phase shifts Θ and Φ , for given beamforming vector \mathbf{w} .

a) Optimizing reflecting and refracting amplitudes and phase shifts Θ_e and Φ_e for ES-IOs

For the ES-IOs, the SI power minimization problem can be formulated as follows:

$$\min_{\Theta_e, \Phi_e} \text{Tr} \left(\left(\mathbf{H}_{tr}^H + \mathbf{H}_{tr}^H \Theta_e \mathbf{H}_{tr} \right) \mathbf{w} \mathbf{w}^H \left(\mathbf{H}_{tr}^H + \mathbf{H}_{tr}^H \Theta_e^H \mathbf{H}_{tr} \right) \right) \quad (46)$$

$$\text{s.t.} \quad \mathbf{h}_{id}^H \Phi_e \mathbf{H}_{ti} \mathbf{w} \mathbf{w}^H \mathbf{H}_{ti}^H \Phi_e^H \mathbf{h}_{id} \geq \left(2^{R_{th}^{DL}} - 1 \right) \sigma_d^2, \quad (46a)$$

$$a_{e,l}^2 + b_{e,l}^2 \leq 1, \quad (46b)$$

$$0 \leq a_{e,l}, b_{e,l} \leq 1, \quad (46c)$$

$$0 \leq \alpha_{e,l}, \beta_{e,l} \leq 2\pi, \quad \forall l. \quad (46d)$$

Following the methodology in maximizing the data rate, we can reformulate the SI power minimization problem as follows:

$$\min_{\alpha_e, \beta_e} \alpha_e^H \Xi_{e,2} \alpha_e + \mathbf{z}_{e,2}^H \alpha_e^* + \alpha_e^T \mathbf{z}_{e,2} \quad (47)$$

$$\text{s.t.} \quad \text{diag} \left\{ \alpha_e \alpha_e^H + \beta_e \beta_e^H \right\} \leq \mathbf{1}_L, \quad (47a)$$

$$2 \text{Re} \left\{ \beta_e^H \Xi_{e,1} \tilde{\beta}_e \right\} \geq \tilde{\beta}_e^H \Xi_{e,1} \tilde{\beta}_e + \left(2^{R_{th}^{DL}} - 1 \right) \sigma_d^2, \quad (47b)$$

which completes the joint amplitudes and phase shifts optimization part for ES-IOs. Note that the algorithm for

Algorithm 3 SI power minimizations for both ES-IOS and MS-IOS

Initialize the beamforming vector \mathbf{w}^0 , the reflecting, refracting amplitudes and phase shifts Θ_e^0, Φ_e^0 of the ES-IOS, the phase shifts of MS-IOS Θ_m^0, Φ_m^0 , as well as the mode selection matrix of MS-IOS \mathbf{A}_m^0 , compute $P_e(\mathbf{w}^0, \Theta_e^0, \Phi_e^0)$ and $P_m(\mathbf{w}^0, \Theta_m^0, \Phi_m^0, \mathbf{A}_m^0)$, respectively. Set $t = 0$ and the accuracy for iteration ε_2 .

repeat

1. Given $\mathbf{w}^t, \mathbf{A}_m^0, \Theta_e^t, \Phi_e^t, \Theta_m^t$ and Φ_m^t , compute the SI powers as $P_e(\mathbf{w}^t, \Theta_e^t, \Phi_e^t)$ and $P_m(\mathbf{w}^t, \Theta_m^t, \Phi_m^t, \mathbf{A}_m^0)$, respectively.
2. Given Θ_e^t, Φ_e^t for the case with ES-IOS and given $\mathbf{A}_m^t, \Theta_m^t$ and Φ_m^t for the case with MS-IOS, optimize \mathbf{w}^{t+1} by solving problem (45).
3. Given \mathbf{w}^{t+1} , optimize Θ_e^{t+1} and Φ_e^{t+1} by solving problem (47) for the ES-IOS. As for the MS-IOS, optimize Θ_m^{t+1} and Φ_m^{t+1} with given \mathbf{w}^{t+1} and \mathbf{A}_m^t for the case with MS-IOS, by solving problem (48).
4. By solving (49) for the case with MS-IOS, optimize \mathbf{X} given $\mathbf{w}^{t+1}, \Theta_m^{t+1}$ and Φ_m^{t+1} .
5. For the case with MS-IOS, retrieve \mathbf{A}_m^{t+1} from \mathbf{X} using Gaussian randomization procedure.
6. Compute the SI powers $P_e(\mathbf{w}^{t+1}, \Theta_e^{t+1}, \Phi_e^{t+1})$ and $P_m(\mathbf{w}^{t+1}, \Theta_m^{t+1}, \Phi_m^{t+1}, \mathbf{A}_m^t)$ for both the IOSs.
7. Set $t = t + 1$.

until $\frac{|P_e(\mathbf{w}^{t+1}, \Theta_e^{t+1}, \Phi_e^{t+1}) - P_e(\mathbf{w}^t, \Theta_e^t, \Phi_e^t)|}{P_e(\mathbf{w}^{t+1}, \Theta_e^{t+1}, \Phi_e^{t+1})} \leq \varepsilon_2$ or $\frac{|P_m(\mathbf{w}^{t+1}, \Theta_m^{t+1}, \Phi_m^{t+1}, \mathbf{A}_m^{t+1}) - P_m(\mathbf{w}^t, \Theta_m^t, \Phi_m^t, \mathbf{A}_m^t)|}{P_m(\mathbf{w}^{t+1}, \Theta_m^{t+1}, \Phi_m^{t+1}, \mathbf{A}_m^{t+1})} \leq \varepsilon_2$.

minimizing the SI power can be found in Algorithm 3.

b) Optimizing reflecting and refracting phase shifts Θ'_m and Φ'_m for ES-IOS

For the case with MS-IOS, following the similarity of the methodology above, the SI power minimization problem can be formulated as follows:

$$\min_{\alpha_m, \beta_m} \alpha_m^H \Xi_{m,2} \alpha_m + \mathbf{z}_{m,2}^H \alpha_m^* + \alpha_m^T \mathbf{z}_{m,2} + d_{m,2} \quad (48)$$

$$\text{s.t. } 2 \operatorname{Re} \left\{ \beta_m^H \Xi_{m,1} \tilde{\beta}_m \right\} \geq \tilde{\beta}_m^H \Xi_{m,1} \tilde{\beta}_m + \left(2^{R_{th}^{DL}} - 1 \right) \sigma_d^2, \quad (48a)$$

$$\operatorname{diag} \left\{ \alpha_m \alpha_m^H \right\} \leq \mathbf{1}_L, \quad (48b)$$

$$\operatorname{diag} \left\{ \beta_m \beta_m^H \right\} \leq \mathbf{1}_L, \quad (48c)$$

which is a quadratically constrained quadratic problem and can be solved by CVX using QCQP method.

C. Optimizing mode selection \mathbf{A}_m with given \mathbf{w} , Θ'_m and Φ'_m for MS-IOS

In this subsection, we aim to optimize the mode selection matrix \mathbf{A}_o with given phase shifts and beamforming vector for the case with MS-IOS. The SI power minimization problem is formulated as follows:

$$\min_{\mathbf{X}} \frac{1}{4} \operatorname{Tr}(\Xi'_{m,2} \mathbf{X}) + c_{m,2} \quad (49)$$

$$\text{s.t. } \frac{1}{4} \operatorname{Tr}(\Xi'_{m,1} \mathbf{X}) + c_{m,1} \geq (2^{R_{th}^{DL}} - 1) \sigma_d^2, \quad (49a)$$

$$\operatorname{diag} \{ \mathbf{X} \} = \mathbf{1}_{L+1}, \quad (49b)$$

which is a convex problem with convex constraints, and shares the similarity as the data rate maximization problem which can be easily solved using the SDR method.

D. Overall Algorithm, convergence and complexity analysis

To sum up, the overall alternative optimization algorithm for minimizing the SI is provided in Algorithm 3. The QCQP method is applied to solve the beamforming vector, reflecting, reflecting joint amplitudes and phase shifts optimizations for the case with ES-IOS, as well as the phase shifts optimization for the MS-IOS. Furthermore, the SDR method and Gaussian randomization procedure are exploited for solving the element mode selection for the case with MS-IOS. Algorithm 3 guarantees the objective function $P_r(\mathbf{w}, \Theta_x, \Phi_x)$ decreases monotonically, therefore, $P_r(\mathbf{w}^{t+1}, \Theta_x^{t+1}, \Phi_x^{t+1}) < P_r(\mathbf{w}^t, \Theta_x^t, \Phi_x^t) < \dots < P_r(\mathbf{w}^0, \Theta_x^0, \Phi_x^0)$, which demonstrates the convergence of the proposed algorithm. Every step in Algorithm 3 guarantees the objective function decreases monotonically, therefore, the convergence of the proposed algorithm is guaranteed. The overall computational complexities of SI minimization problem for the cases with ES-IOS and MS-IOS are $\mathcal{O}(N_{ite} \times \max\{M^3, L^3\})$ and $\mathcal{O}(N_{ite} \times \max\{M^3, L^{3.5}, G\})$, respectively.

V. NUMERICAL RESULTS

In this section, simulation results are provided to demonstrate the performance of the proposed optimization methods. The 3-dimensional coordinates of the destination, the first transmit antenna, the first receive antenna, and the first element at the IOS are set as $[15, -10, 1.5]$, $[0, 0, 5]$, $[0, 1, 5]$ and $[0.1, 0, 5]$ m, respectively. In addition, $\lambda = 0.05$ m and the distance between any two adjacent elements/antennas is $\frac{\lambda}{2}$, the Rician path-loss exponent and Rician factor are $\kappa = 2.5$ and $K = 3$ dB, respectively. The noise powers at the destination and transmitter are $n_d = n_r = -90$ dBm, the uplink and downlink data rate thresholds R_{th}^{UL} and R_{th}^{DL} for the optimizations are $0 \sim 4$ and $0 \sim 3$ bps/Hz, respectively. Furthermore, the length of the Gaussian randomization procedure $G = 10^3$, and the convergence thresholds are set to $\varepsilon_1 = \varepsilon_2 = 10^{-5}$. Specifically, we compare the performance of our proposed algorithms with the following three schemes:

- 1) **WO-IOS**: In this scheme, only the beamforming vectors of the transmit signals are optimized in the proposed system without the assistance of IOS. This scheme is set as the benchmark for performance evaluation.
- 2) **ES-IOS**: The ES-IOS is employed to assist signal transmission and SI mitigation; specifically, the beamforming vectors of the transmitter, as well as the reflecting and refracting phase shifts of the ES-IOS, are designed using the QCQP method.
- 3) **MS-IOS**: Compared with the ES-IOS, each element of the MS-IOS can either reflect or refract signals in the one-time slot; therefore, the beamforming vectors, both the reflecting and the refracting phase shifts, jointly with the mode selection, are optimized for the proposed system.

Fig. 2 shows the data rate convergence behaviours of the proposed joint optimization method with uplink rate threshold $R_{th}^{UL} = 0.5$ bps/Hz, number of elements $L = 128$ and different numbers of receive antenna N for the three schemes. It is shown that the downlink rates of all schemes converge

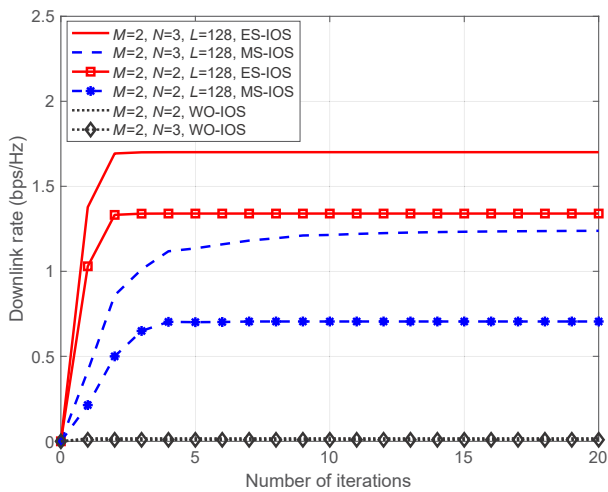


Fig. 2. Iteration behaviour of the downlink rate maximization problem with the three schemes.

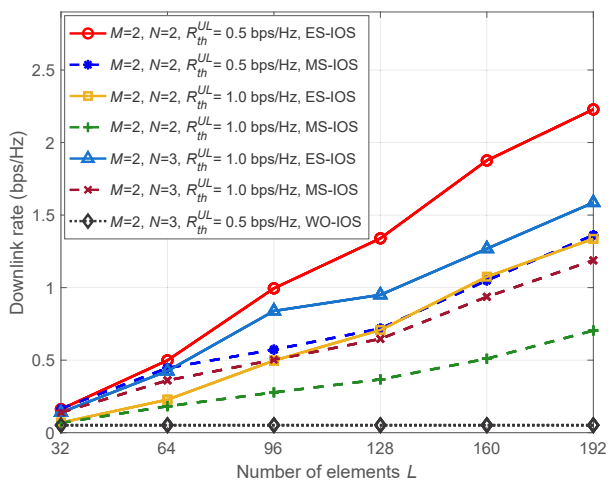


Fig. 3. Downlink rate performance of the three schemes with different L and N .

fast with the proposed algorithms, which demonstrates their efficiency. Furthermore, the downlink rates increase with N , this is because as the number of receive antennas increases, the uplink transmission benefits from the channel diversity. It is evident that both ES-IOS and MS-IOS outperform WO-IOS in performance due to the degrees of freedom bestowed by the IOSs. Besides, the rates with MS-IOS are lower than that of ES-IOS because each element of the MS-IOS can only reflect or refract signals at one time, and it can not fully exploit the reflecting and refracting resource as ES-IOS does.

The comparison of data rates with different numbers of elements L , different numbers of receive antennas N and different R_{th}^{UL} is illustrated in Fig. 3. As we can see, to guarantee the SI power above a threshold $R_{th}^{UL} = 0.5$ bps/Hz, the case with WO-IOS can not achieve a high downlink rate. In addition, it can be noticed that the data rates with ES-IOS and MS-IOS increase with the number of elements, and the performance of ES-IOS is better than that of MS-IOS. Significant improvement can be achieved by introducing ES-

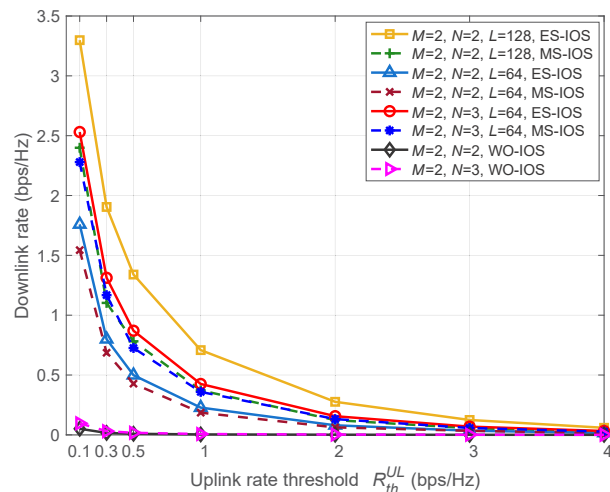


Fig. 4. Downlink rate performance of the three schemes with different uplink rate threshold R_{th}^{UL} .

IOS or MS-IOS into FD wireless communication networks; for example, 2.23 and 1.36 bps/Hz can be obtained with ES-IOS and MS-IOS, respectively, when $L = 192$, $M = 2$ and $N = 2$. However, without the assistance of an IOS, only the beamforming can be designed to mitigate the SI; thus, only 0.02 bps/Hz can be achieved even with $N = 3$. In addition, the data rates with $R_{th}^{UL} = 1$ bps/Hz are smaller compared with $R_{th}^{UL} = 0.5$ bps/Hz due to the stringent uplink transmission requirement, e.g. 0.71 bps/Hz with $L = 128$, $M = 2$, $N = 2$ for ES-IOS case, around 47% smaller than the former case. Fig. 4 illustrates the data rate performance of the proposed algorithm with $L = 64/128$ and different uplink rate thresholds for the three schemes. It can be noticed that the data rates degrade quickly with the uplink rate thresholds for ES-IOS and MS-IOS. As we can see, the downlink rates with IOSs are very competitive when $R_{th}^{UL} = 0.1$ to 0.5 bps/Hz. Also, the degree of freedom brought by the ES-IOS and MS-IOS boosts the data rate significantly compared to the case without an IOS. Furthermore, the cases without an IOS are introduced for comparison; both downlink rates with $N = 2$ and $N = 3$ are much lower than that with ES-IOS and MS-IOS. Moreover, the performance gap between the ES-IOS and MS-IOS is not obvious as the distance increases since the channel gains between the IOSs and the antennas degrade, rendering the limited abilities of self-interference cancellation via both ES-IOS and MS-IOS.

In addition, the impact of the distances between transmit and receive antennas on the data rate is shown in Fig. 5, where $R_{th}^{UL} = 0.5$ bps/Hz is considered. It is shown that the downlink rates of the proposed schemes benefit from antenna isolation, by increasing the distance from 0.2 m to 1 m with different L and N in the proposed system. Using the IOS will guarantee transmission and reflection beam patterns are the dominant factors to balance the tradeoff between the downlink rates and uplink rates against the distance's effect. Also, it is evident that for all curves, the data rates with the ES-IOS case are larger than that with the MS-IOS case.

Fig. 6 illustrates the impact of the distance between the

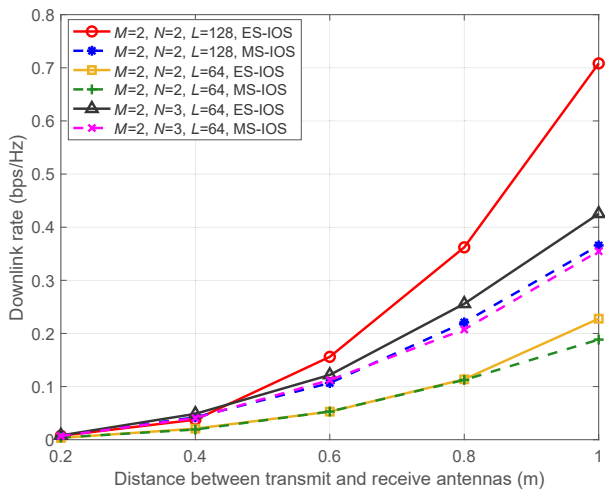


Fig. 5. The impact of the distance between transmit and receive antennas on the data rates.

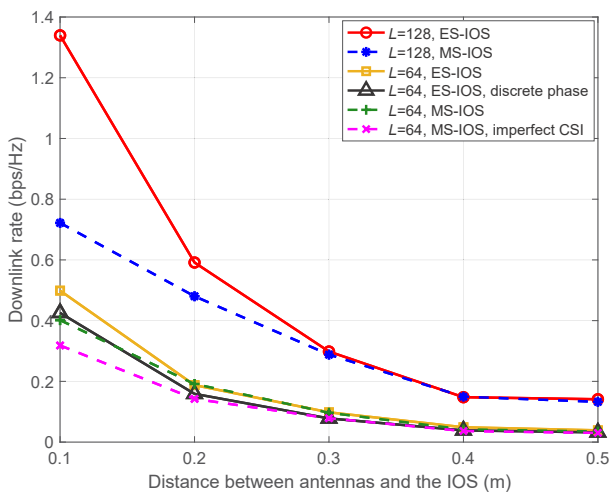


Fig. 6. The impact of the distance between transmitter and IOSs on the data rates.

transmitter and IOSs on the data rates, where $M = N = 2$. The curves clearly show that the data rates decrease with the distance between the transmitter and IOSs. This is because as the distance increase, the channel gains between transmit and the IOS are weakened by propagation, rendering the limited ability of the IOS to mitigate the SI at the transmitter. Furthermore, the data rates with continuous phase shifts slightly outperform the discrete phase shifts with 4 bits quantization with $M = 2$, $N = 2$ and $L = 64$ for the ES-IOS case, e.g. 0.5 bps/Hz with continuous phase shifts compared to 0.43 bps/Hz with discrete phase shifts. Also, for the case of imperfect channel estimation, we define the estimated channels between the IOSs and destination, the transmit and receive antennas as $\hat{\mathbf{h}}_{id} = \sqrt{\eta}\mathbf{h}_{id} + \sqrt{1-\eta}\Delta\mathbf{h}_{id}$ and $\hat{\mathbf{H}}_{tr} = \sqrt{\eta}\mathbf{H}_{tr} + \sqrt{1-\eta}\Delta\mathbf{H}_{tr}$, where $\eta \in [0, 1]$ represents the estimation accuracy, $\Delta\mathbf{h}_{id}$ and $\Delta\mathbf{H}_{tr}$ are the estimation errors, which have the same statistical properties as of \mathbf{h}_{id} and \mathbf{H}_{tr} in terms of mean and variance values. The rate performance loss can be observed when imperfect CSI is considered for MS-IOS case with $M = 2$,

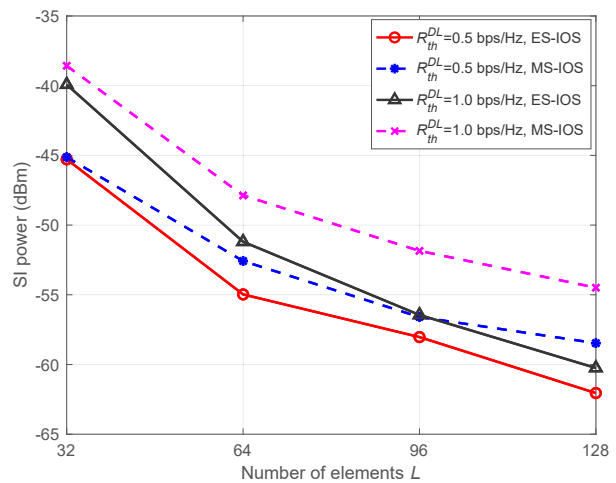


Fig. 7. SI power performance of the three schemes with different L and R_{th}^{DL} .

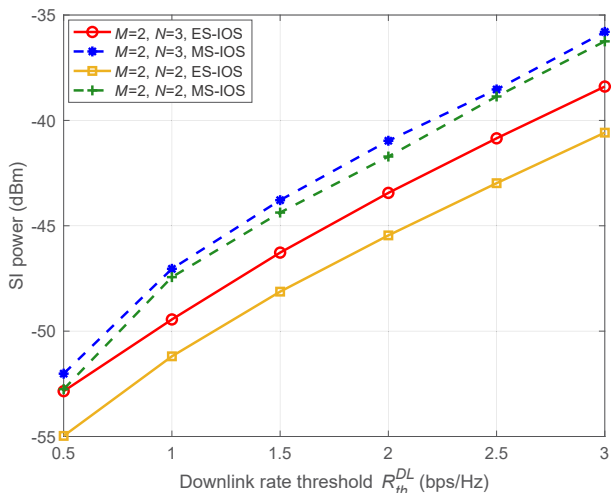


Fig. 8. SI power performance of the three schemes with different data rate threshold R_{th} .

$N = 2$ and $\eta = 0.95$, for example, 0.32 bps/Hz compared to 0.40 bps/Hz with perfect CSI when the distance between the transmitter and the IOS is 0.1 m.

The performance of the SI power minimization concerning different R_{th}^{DL} and different numbers of elements L is shown in Fig. 7, where $M = N = 2$. The data rate threshold $R_{th} = 0.5$ and 1 bps/Hz are introduced for both ES-IOS and MS-IOS. It is obvious that all the SI powers of ES-IOS and MS-IOS can be effectively reduced by increasing the number of elements. For example, the SI power can be reduced to around -62 dBm by employing 128 IOS elements even when the numbers of transmit and receive antennas are limited, with $M = 2$ and $N = 2$ or 3. However, the SI powers of $L < 96$ with $R_{th}^{DL} = 1$ bps/Hz is still large for both ES-IOS and MS-IOS, the reason for it is to meet a certain rate threshold with small L , a large proportion of the IOS elements should fully participate in increasing the downlink rate, thus renders high SI. Furthermore, the SI powers with MS-IOS are larger than that with ES-IOS, e.g. -58.5 dBm for MS-IOS compared to

−62 dBm for ES-IOS with $M = 2$, $N = 2$, $L = 128$ and $R_{th} = 0.5$ bps/Hz. In addition, it is evident that SI powers with $R_{th} = 0.5$ bps/Hz for both IOSs are smaller than that with $R_{th} = 1$ bps/Hz, and it can be noticed that fewer receive antennas lead to higher SI powers. Nevertheless, even with a high rate requirement, both IOSs are still capable of achieving the required data rate, as well as reducing the SI power to a limited region, via deploying more reflecting and refracting elements.

Fig. 8 shows the SI powers at the transmitter with different N and different downlink rate thresholds for the cases with ES-IOS and MS-IOS, where $L = 64$. It can be observed that a higher downlink rate requirement would lead to higher residual SI power, and the SI mitigation performance with ES-IOS is slightly better than that with MS-IOS. In theory, the MS-IOS can be regarded as a special case of the ES-IOS, by considering the reflecting and refracting amplitudes of the ES-IOS in (1a) as integers (0 or 1), therefore, the ES-IOS outperforms the MS-IOS. Also, it is evident that the number of receive antennas impacts the SI power significantly in the proposed FD wireless communication system.

VI. CONCLUSION

In this paper, we proposed a new IOS-assisted FD MISO implementation, which solved the frequency-dependent and SWaP limitation in the traditional FD scheme by completely bypassing the analogue SIC. To maximize the data rate at the destination and minimize SI power received at the antennas, beamforming vectors at the transmitter, the phase shifts, and mode selection optimizations of ES-IOS and MS-IOS were conducted. However, both the formulated problems were non-convex and intractable due to the coupling of the variables. Alternative optimization algorithms were designed to circumvent this issue to solve the problems iteratively. Specifically, the QCQP method was applied to solve the beamforming vectors and the phase shifts for ES-IOS cases. On the other hand, the mode selection optimization for the case with MS-IOS was still intractable. Hence, we resorted to the SDR and Gaussian randomization procedure to solve it. Furthermore, the first-order Taylor expansions were leveraged to convexify the non-convex constraints for the optimization problems. The simulation results demonstrated the efficacy of the proposed algorithms and the flexibility of utilizing the IOSs for trading off the SIC and data transmission. The applications of IOS in FD communication networks with multiple users and transmitters, and the maximization of the uplink transmission rate will be left as our future work.

APPENDIX A DERIVATIONS OF (37) AND (38)

With the binary variable $\mathbf{b} = 2\mathbf{a}_m - \mathbf{1}_L$, the objective function of the data rate maximization problem can be reformulated

as follows:

$$\begin{aligned} & \mathbf{a}_m^T \Xi_{m,1} \mathbf{a}_m - 2 \operatorname{Re} \left\{ \mathbf{a}_m^T \mathbf{w}_{m,1} \right\} + d_{m,1} \\ & = \mathbf{a}_m^T \Xi_{m,1} \mathbf{a}_m + 2 \operatorname{Re} \left\{ \mathbf{a}_m^T (-\mathbf{w}_{m,1}) \right\} + d_{m,1} \\ & = \left(\frac{\mathbf{1}_L + \mathbf{b}}{2} \right)^T \Xi_{m,1} \left(\frac{\mathbf{1}_L + \mathbf{b}}{2} \right) + d_{m,1} \\ & \quad + 2 \operatorname{Re} \left\{ \left(\frac{\mathbf{1}_L + \mathbf{b}}{2} \right)^T (-\mathbf{w}_{m,1}) \right\} \\ & = \frac{1}{4} \operatorname{Tr} (\Xi_{m,1} \mathbf{B}) + \frac{1}{4} \operatorname{Tr} (\Xi_{m,1}) + \frac{1}{2} \operatorname{Tr} (\Xi_{m,1} \mathbf{1}_L \mathbf{b}^T) \\ & \quad + \operatorname{Re} \left\{ \mathbf{b}^T (-\mathbf{w}_{m,1}) \right\} + \operatorname{Re} \left\{ \mathbf{1}_L^T (-\mathbf{w}_{m,1}) \right\} + d_{m,1} \\ & = \frac{1}{4} \left(\operatorname{Tr} (\Xi_{m,1} \mathbf{B}) + 2 \operatorname{Re} \left\{ \mathbf{h}^T \mathbf{b} \right\} \right) + c_{m,1}, \end{aligned} \quad (50)$$

where $\mathbf{B} = \mathbf{b} \mathbf{b}^T$, $\mathbf{h} = -2\mathbf{w}_{m,1} + \mathbf{h}_{m,1}$, and

$$\mathbf{h}_{m,1} = \left[\sum_{i=1}^L [\Xi_{m,1}]_{1,i}; \sum_{i=1}^L [\Xi_{m,1}]_{2,i}; \dots; \sum_{i=1}^L [\Xi_{m,1}]_{L,i} \right]^T, \quad (51)$$

$$c_{m,1} = \frac{1}{4} \operatorname{Tr} (\Xi_{m,1}) + \operatorname{Re} \left\{ \mathbf{1}_L^T (-\mathbf{w}_{m,1}) \right\} + d_{m,1}. \quad (52)$$

Similarly, we can obtain the SI power function as follows:

$$\frac{1}{4} \left(\operatorname{Tr} (\Xi_{m,2} \mathbf{B}) + 2 \operatorname{Re} \left\{ \mathbf{g}^T \mathbf{b} \right\} \right) + c_{m,2}, \quad (53)$$

where

$$\mathbf{g} = 2\mathbf{w}_{m,2} + \mathbf{h}_{m,2}, \quad (54)$$

$$\mathbf{h}_{m,2} = \left[\sum_{i=1}^L [\Xi_{m,2}]_{1,i}; \sum_{i=1}^L [\Xi_{m,2}]_{2,i}; \dots; \sum_{i=1}^L [\Xi_{m,2}]_{L,i} \right]^T, \quad (55)$$

$$c_{m,2} = \frac{1}{4} \operatorname{Tr} (\Xi_{m,2}) + \operatorname{Re} \left\{ \mathbf{1}_L^T (-\mathbf{w}_{m,2}) \right\} + d_{m,2}. \quad (56)$$

Then by introducing another binary variable $\mathbf{x} = [\mathbf{b}; \mathbf{1}]^T$, we can reformulate the objective function and SI power as follows:

$$\frac{1}{4} \operatorname{Tr} (\Xi'_{m,1} \mathbf{X}) + c_{m,1}, \quad (57)$$

$$\frac{1}{4} \operatorname{Tr} (\Xi'_{m,2} \mathbf{X}) + c_{m,2}, \quad (58)$$

respectively, where $\Xi'_{m,1} = \begin{bmatrix} \Xi_{m,1} & \mathbf{h} \\ \mathbf{h}^T & 0 \end{bmatrix}$, $\Xi'_{m,2} = \begin{bmatrix} \Xi_{m,2} & \mathbf{g} \\ \mathbf{g}^T & 0 \end{bmatrix}$ and $\mathbf{X} = \mathbf{x} \mathbf{x}^T$, which completes the derivation.

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